## AIR DENSITY AND ITS UNCERTAINTY

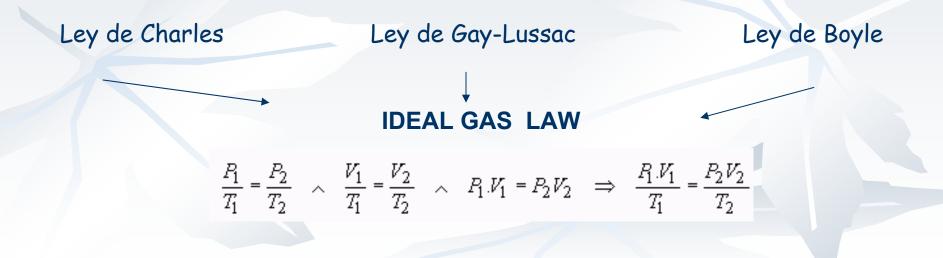
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## Air and its composition

The dry air as the water steam behaves like ideal gases. They have been developed to empirical laws that relate the macroscopic values, in ideal gases, these values include pressure (p), volume (V) and temperature (T)



## Air and its composition

- It is constituted by a nitrogen mixture and of oxygen like basic element (99%) and the rest like noble gases. The composition is similar around the world.
- Water Steam (0-5%), Carbon dioxide, hydrocarbons, tars, ashes, dust and SO2.
- Electrical delivery form C2H2, H202, 03, NO3H, NH3, NO3NH4.

	COMPOSICION DEL AIRE PURO	
	Proporción	Proporción
Elemento	en volumen	en peso
Nitrógeno	78,14	75,6
Oxigeno	20,92	23,1
Argón	0,94	0,3
Neón	1,5 10 <sup>-3</sup>	1 10 <sup>-3</sup>
Helio	5 10 <sup>-4</sup>	0,7 10 <sup>-4</sup>
Criptón	1 10 <sup>-4</sup>	3 10 <sup>-4</sup>
Hidrogeno	5 10 <sup>-5</sup>	0,35 10 <sup>-5</sup>
Xenón	1 10 <sup>-5</sup>	4 10 <sup>-5</sup>

# Ways to calculate the air density

Density defined in a qualitative manner as the measure of the relative mass of objects with a constant volume

$$\delta = \frac{m}{V}$$

Hypothesis de Avogadro Two gases same volume (same pressure and temperature) contain the same number of particles, or molecules

Standard Law gases

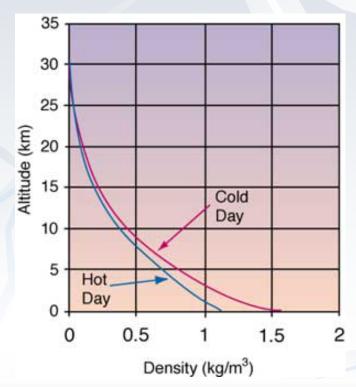
$$P.V = \frac{m}{Mr} R.T \Longrightarrow P.Mr = \frac{m}{V} R.T \Longrightarrow P.Mr = \delta.R.T$$

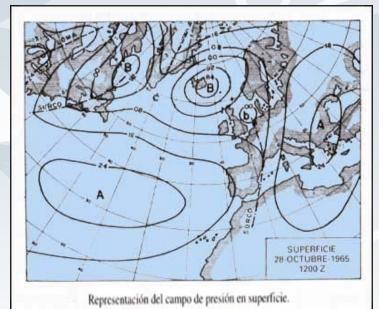
# Ways to calculate the air density

As function of altitude
Using a refractometer
Air buoyancy artefacts methods
Equation CIPM /81
Approximate equation

## Ways to calculate the air density AS FUNCTION OF ALTITUDE

Atmospheric pressure drops about or about 1.1 mbar (kPa) for each 100 meters. Density decreases





## Ways to calculate the air density AS FUNCTION OF ALTITUDE

L = 6,5 temperature lapse rate, deg K/km H = geopotencial altitude Z = geometrical altitude To = Temperature °K Po = Atmospheric Pressure  $T = T_n - L \cdot H$ 



## Ways to calculate the air density REFRACTROMETRY

Changes in air density can be determined with good precision using an optical method based on the high correlation between air density and air index of refraction.

$$\rho = \frac{2}{3R'}(n-1),$$

R specific refraction or the refractional invariant in unction composition of air and the local atmospheric conditions

$$n = \frac{V_{vacio}}{V_{aire}}$$

n is determined by a simple ratio of laser frequencies:

 ${m V}_{vacio}$  laser frequency locked to one transmission peak of the interferometer under vacuum

Vaire the frequency locked to the same peak of the interferometer placed in air.

## Ways to calculate the air density AIR BUOYANCY ARTEFACTS METHODS

The method is based on the weighing of two artefacts having the same nominal mass and the same surface area but with very different volumes. Two weightings are necessary to determine the air density  $\rho$ , one in air and one in vacuum

$$\Delta m_{aire} = I_1 - I_2 + \rho (V_{m1} - V_{m2})$$

I<sub>1</sub> e I<sub>2</sub> balance readings in air mass 1 and mass<sub>2</sub>  $V_{m1} e V_{m2}$  volume of m 1 y m 2  $\rho$  air density  $\Delta m_{vacio} = I_3 - I_4$ 

 $I_3 e I_4$  the balance readings in vacuum mass 1 y mass 2

$$\Delta m_{aire} = \Delta m_{vacio} + \sigma \Delta S$$

•  $\Delta S$  the difference in surface area between the two artefacts and  $\sigma$  mass of adsorption per unit area.

$$\rho = \frac{I_3 - I_4 - (I_1 - I_2 - \sigma \Delta S)}{V_{m1} - V_{m2}}$$

## Ways to calculate the air density FORMULA CIPM

From the equation of state of a non-ideal gas and the experimental conditions the density of moist air

$$\rho_{\rm a} = \frac{pM_{\rm a}}{ZRT} \left[ 1 - x_{\rm v} \left( 1 - \frac{M_{\rm v}}{M_{\rm a}} \right) \right]$$

$$M_{a} = [28,9635 + 12,011(x_{co_{2}} - 0,0004)] * 10^{-3} kgmol^{-1}$$
$$x_{v} = hf(p,t) \frac{p_{sv}(t)}{p}$$

Where

P pressure T thermodynamic temperature 273,15 + t Mv molar mass of the water Z compressibility factor R molar gases constant Ways to calculate the air density APPROXIMATE EQUATION From BIPM formula we obtain one numerical approximate equation :

$$\rho_a = \frac{0,34848 * p - 0,009024 * h_r * e^{0,0612*t}}{273.15 + t}$$

Thermodynamic properties of mixtures of gas with vapor. saturation pressure and temperature of dew, Indexes of humidity, Volume, heat and humid enthalpy, temperature of saturation adiabatic and wet thermometer.

#### Some definitions:

**Relative Humidity**. The relative humidity is the percent of saturation humidity, generally calculated in relation to saturated vapor density, in (%):

#### HR = 100 Pv/Ps (%)

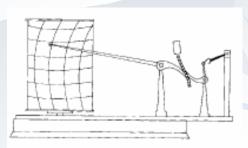
Temperature of adiabatic saturation, Th, is the ideal temperature of equilibrium will have the air non saturated after undergoing an adiabatic and isobaric process (iso enthalpic), that it takes it temperature to the saturation by means of liquid evaporation of water to this.

Temperature of wet thermometer is the temperature that it reaches a thermometer covered with a wet cloth that is exposed to an airflow without saturating that it flows at speeds near 5 m/s

**Dew point** is the temperature, at which the moisture content in the air will saturate the air . If the air is cooled further, some of the moisture will condense.

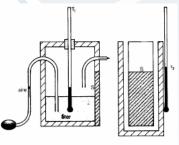
#### To mesure the humidity :

ARTEFACT	METHOD
psychrometer	Thermodynamic
hygrometer of hair or others materials	Hygroscopic
Hygrometer of dew point	Condensation
Hygrometer of Chemist absorption	Gravimetric
Hygrometer digital	Variation of electrical properties

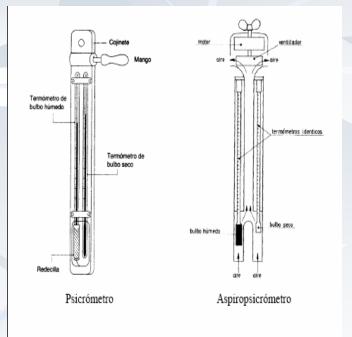


#### Higrógrafo de cabello





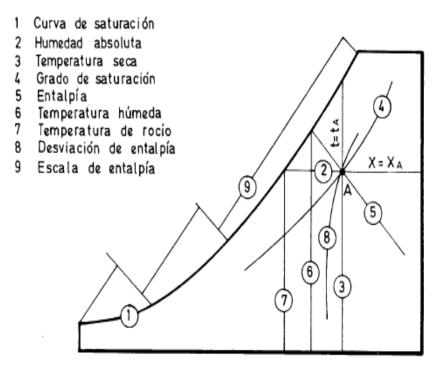
Esquema del higrómetro de punto de rocío.



Psychrometer and aspiro psychrometer Consist two thermometers, one normal (dry) and another with their bulb permanently humidified thanks to a cloth or wet gauze that it recovers it. The humidity can be measured between both starting from the difference of temperature apparatuses

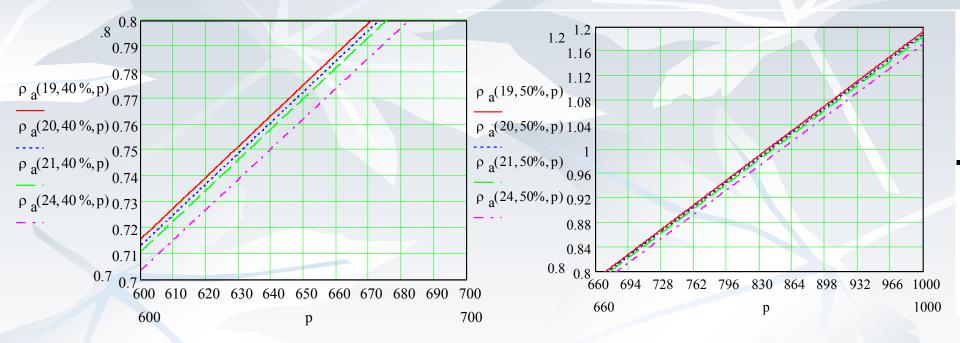
#### Diagram Carrier.

- The T represents (°C) in the abscissa axis (axis x) and the mixture reason or humidity (X, in kg of water/kg of dry air) in the axis of orderly (axis and, to the right).
  - The saturation curve (HR = 100%) it ascends toward the right and it represents the end of the diagram. In this curve the temperatures of humid thermometer and the temperatures of dew are located.
    - The curves of humidity relative constant are similar to that of saturation, advancing down (lying down more) as it diminishes the humidity of the air.



Esquema del diagrama Carrier

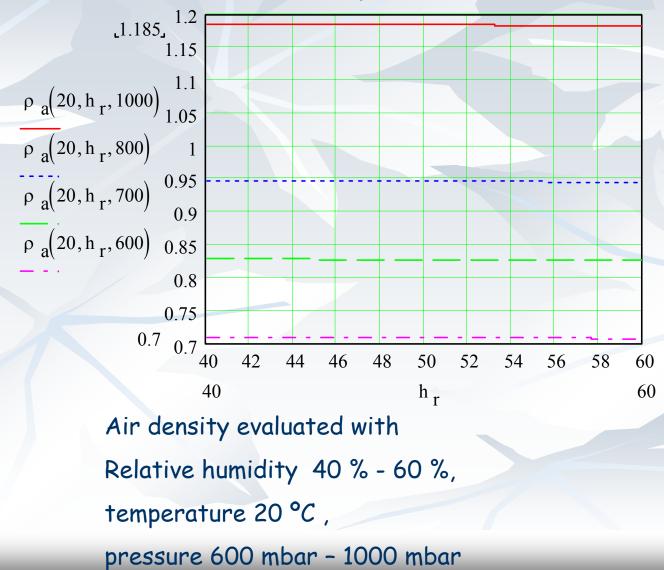
## Ways to calculate the air density CHART



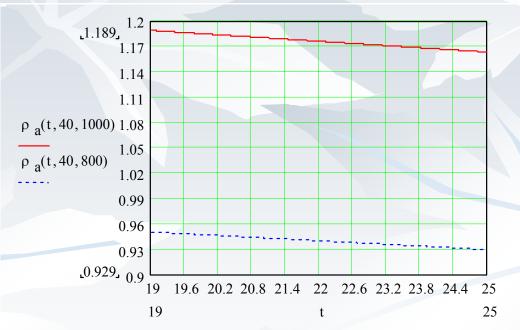
#### Air density evaluated with

Relative humidity 40 %, temperature 19 °C - 24 °C, pressure 600 mbar - 700 mbar Air density with evaluated with Relative humidity 50 %, temperature 19 °C - 24 °C, pressure 660 mbar - 1000 mbar

## Ways to calculate the air density CHART



## Ways to calculate the air density CHART



Air density evaluated with Relative humidity 40 %, temperature 19 °C - 25 °C, pressure 800 mbar - 1000 mbar

## CALCULATION OF THE AIR DENSITY CIPM

$$\frac{pM_a}{ZRT} \left[ 1 - x_v \left( 1 - \frac{M_v}{M_a} \right) \right]$$

Pressure of air in Pa.
molar mass of dry air.
Compressibility factor
Universal constant of ideal gases
Temperature of air in K
molar fraction of water steam
molar mass of water

Molar mass of dry air, Ma
 If it considers constant of air component

 $M_a = 0,028963 512440 \text{ kg} \cdot \text{mol}^{-1}$ 

If it can measure the concentration of  $CO_2$ 

 $M_{a} = [28,9635 + 12,011 (X_{CO2} - 0,0004)]* 10^{-3} \text{ kg} \cdot \text{mol}^{-1}$ 

• Compressibility factor, Z

$$Z = 1 - \frac{p}{T} \Big[ a_0 + a_1 t + a_2 t^2 + (b_0 + b_1 t) x_v + (c_0 + c_1 t) x_v^2 \Big] + \frac{p^2}{T^2} \Big( d + e x_v^2 \Big)$$

Where:

Air pressure in Pa р Air temperature in K T Environmental temperature in °C t 1, 581 23 X 10<sup>-6</sup> K Pa<sup>-1</sup>  $a_0$ -2,9331 x 10-8 Pa-1  $\mathbf{a}_1$ 1,1043 x 10<sup>-10</sup> K<sup>-1</sup> Pa<sup>-1</sup>  $a_2$ 5,707 x 10-6 K Pa-1  $\mathbf{b}_0$ -2,051 X 10-8 Pa-1  $\mathbf{b}_1$ 1.9898 x 10<sup>-4</sup> K Pa<sup>-1</sup>  $\mathbf{C}_{0}$  $\mathbf{C}_1$ - 2,376 x 10<sup>-6</sup> Pa<sup>-1</sup> d 1,83 x 10-11K<sup>2</sup>Pa<sup>-2</sup> -0,765 x 10-8 K<sup>2</sup>Pa-<sup>2</sup> e

- Universal Constant of ideal gases, R  $R = 8.314510 \pm 8.4 \text{ x lO-6 J} \cdot \text{mol}^{-1} \cdot \text{K}^{-1}$
- Molar fraction of water steam, Xv
   In function of relative humidity, h

$$x_v = hf(p,t)\frac{p_{sv}(t)}{p}$$

In function of temperature of dew point, tr

$$X_{v} = f(p, t_{r}) \frac{p_{sv}(t_{r})}{p}$$

#### Where:

- *h* Relative humidity
- $P_{sv}$  Pressure of saturated steam
- $f(p,t_r)$  Fugacity factor

## **Enhancement factor f f(p,t**,)

$$f = \alpha + \beta p + \gamma t^2$$

Where:

p

T

- - Air pressure in Pa
    - Air temperature in  $^{O}C$  or dew point temperature (t<sub>r</sub>) in  $^{O}C$

#### Pressure of saturated steam, p<sub>sv</sub>

$$p_{sv} = 1Pax \exp\left[AT^2 + BT + C + \frac{D}{T}\right]$$

#### Where:

A 1,237 884 7 x 10-5 K-2
B -1,912 131 6 x 10-2 K-1
C 33,937 110 47
D -6,343 164 5 x 103 K
T Air temperature in K or temperature (Tr) in K

dew point

**UNCERTAINTY OF AIR DENSITY** 

#### SOURCES OF UNCERTAINTY

**Atmospheric temperature** 

$$up = \sqrt{u_{p1}^2 + u_{p2}^2 + u_{p3}^2}$$

• Calibration of barometric

$$u_{p1} = \frac{U_B}{k}$$

 $u_{p2}$ 

Resolution of barometric

• Variation of atmospheric pressure during calibration

$$up3 = \frac{p^+ - p^-}{\sqrt{24}}$$

 $d_{B}$ 

#### **Environmental conditions**

$$u_t = \sqrt{u_{t1}^2 + u_{t2}^2 + u_{t3}^2}$$

Calibration of thermometer

 $u_{t1} = \frac{U_t}{k}$ 

Resolution of instrument

 $u_{t2} = \frac{d_t}{\sqrt{12}}$ 

 Variation of temperature during calibration

 $u_{t3} = \frac{t^+ - t^-}{\sqrt{24}}$ 

#### **Relative humidity of air**

$$u_h = \sqrt{u_{h1}^2 + u_{h2}^2 + u_{h3}^2}$$

Calibration of hygrometer

$$u_{h1} = \frac{U_h}{k}$$

• Resolution of hygrometer

$$u_{h2} = \frac{d_h}{\sqrt{12}}$$

• Variation of the air relative humidity during calibration

$$u_{h3} = \frac{h^+ - h^-}{\sqrt{24}}$$

**Constant R of ideal gases** 

 $u_R = 84x \ 10^{-7} \ J \ mol^{-1} \ K^{-1}$ 

Equation adjustment for the determination of air density

 $u_{ec} = (1x10^{-4})(0,9495) = 9,50x10^{-5} kgm^{-3}$ 

#### **Sensitivity Coefficient**

#### Pressure

$$c_{p} = \left[\frac{\partial \rho_{a}}{\partial p} + \left(\frac{\partial \rho_{a}}{\partial Z}\frac{\partial Z}{\partial p}\right) + \left(\frac{\partial \rho_{a}}{\partial Z}\frac{\partial Z}{\partial X_{v}}\frac{\partial X_{v}}{\partial f}\frac{\partial f}{\partial p}\right) + \left(\frac{\partial \rho_{a}}{\partial Z}\frac{\partial Z}{\partial X_{v}}\frac{\partial X_{v}}{\partial p}\right) + \left(\frac{\partial \rho_{a}}{\partial X_{v}}\frac{\partial X_{v}}{\partial f}\frac{\partial f}{\partial p}\right) + \left(\frac{\partial \rho_{a}}{\partial X_{v}}\frac{\partial X_{v}}{\partial p}\right) = \left(\frac{\partial \rho_{a}}{\partial X_{v}}\frac{\partial X_{v}}{\partial f}\frac{\partial f}{\partial p}\right) + \left(\frac{\partial \rho_{a}}{\partial X_{v}}\frac{\partial X_{v}}{\partial p}\right) = \left(\frac{\partial \rho_{a}}{\partial X_{v}}\frac{\partial X_{v}}{\partial f}\frac{\partial f}{\partial p}\right) + \left(\frac{\partial \rho_{a}}{\partial X_{v}}\frac{\partial X_{v}}{\partial p}\right) = \left(\frac{\partial \rho_{v}}{\partial X_{v}}\frac{\partial X_{v}}{\partial p}\right) = \left(\frac{\partial \rho_{v}}^{v}(x)\right) = \left(\frac{\partial \rho$$

#### Temperature

$$ct = \begin{bmatrix} \left(\frac{\partial\rho_{a}}{\partial Z} \cdot \frac{\partial Z}{\partial T} \cdot \frac{\partial T}{\partial t}\right) + \left(\frac{\partial\rho_{a}}{\partial Z} \cdot \frac{\partial Z}{\partial t}\right) + \left(\frac{\partial\rho_{a}}{\partial Z} \cdot \frac{\partial Z}{\partial X_{v}} \cdot \frac{\partial X_{v}}{\partial f} \cdot \frac{\partial f}{\partial t}\right) + \left(\frac{\partial\rho_{a}}{\partial Z} \cdot \frac{\partial X_{v}}{\partial Y_{v}} \cdot \frac{\partial F_{sv}}{\partial t} \cdot \frac{\partial F_{sv}}{\partial t}\right) + \left(\frac{\partial\rho_{a}}{\partial X_{v}} \cdot \frac{\partial F_{sv}}{\partial f} \cdot \frac{\partial F_{sv}}{\partial t}\right) + \left(\frac{\partial\rho_{a}}{\partial X_{v}} \cdot \frac{\partial F_{sv}}{\partial f} \cdot \frac{\partial F_{sv}}{\partial t}\right) + \left(\frac{\partial\rho_{a}}{\partial X_{v}} \cdot \frac{\partial F_{sv}}{\partial F_{sv}} \cdot \frac{\partial F_{sv}}{\partial T} \cdot \frac{\partial F_{sv}}{\partial t}\right) + \left(\frac{\partial\rho_{a}}{\partial X_{v}} \cdot \frac{\partial F_{sv}}{\partial F_{sv}} \cdot \frac{\partial F_{sv}}{\partial T} \cdot \frac{\partial F_{sv}}{\partial t}\right) + \left(\frac{\partial\rho_{a}}{\partial X_{v}} \cdot \frac{\partial F_{sv}}{\partial F_{sv}} \cdot \frac{\partial F_{sv}}{\partial T} \cdot \frac{\partial F_{sv}}{\partial t}\right) + \left(\frac{\partial\rho_{sv}}{\partial X_{v}} \cdot \frac{\partial F_{sv}}{\partial F_{sv}} \cdot \frac{\partial F_{sv}}{\partial T} \cdot \frac{\partial F_{sv}}{\partial t}\right) + \left(\frac{\partial\rho_{sv}}{\partial X_{v}} \cdot \frac{\partial F_{sv}}{\partial F_{sv}} \cdot \frac{\partial F_{sv}}{\partial T} \cdot \frac{\partial F_{sv}}{\partial t}\right) + \left(\frac{\partial\rho_{sv}}{\partial X_{v}} \cdot \frac{\partial F_{sv}}{\partial F_{sv}} \cdot \frac{\partial F_{sv}}{\partial T} \cdot \frac{\partial F_{sv}}{\partial t}\right) + \left(\frac{\partial\rho_{sv}}{\partial F_{sv}} \cdot \frac{\partial F_{sv}}{\partial F_{sv}} \cdot \frac{\partial F_{sv}}{\partial T} \cdot \frac{\partial F_{sv}}{\partial t}\right) + \left(\frac{\partial\rho_{sv}}{\partial F_{sv}} \cdot \frac{\partial F_{sv}}{\partial F_{sv}} \cdot \frac{\partial F_{sv}}{\partial T} \cdot \frac{\partial F_{sv}}{\partial T}\right) + \left(\frac{\partial\rho_{sv}}{\partial F_{sv}} \cdot \frac{\partial F_{sv}}{\partial F_{sv}} \cdot \frac{\partial F_{sv}}{\partial T} \cdot \frac{\partial F_{sv}}{\partial T}\right) + \left(\frac{\partial\rho_{sv}}{\partial F_{sv}} \cdot \frac{\partial F_{sv}}{\partial F_{sv}} \cdot \frac{\partial F_{sv}}{\partial T} \cdot \frac{\partial F_{sv}}{\partial F_{sv}} \cdot$$

**Relative humidity.** 

$$C_{h} = \left[ \left( \frac{\partial \rho_{a}}{\partial Z} \cdot \frac{\partial Z}{\partial X_{v}} \cdot \frac{\partial X_{v}}{\partial h} \right) + \left( \frac{\partial \rho_{a}}{\partial X_{v}} \cdot \frac{\partial X_{v}}{\partial h} \right) \right]$$

## Where:

$$\frac{\partial T}{\partial t} = \frac{1}{2}$$

$$\frac{\partial P_{sv}}{\partial T} = \left[ \exp\left(AT^2 + BT + C + \frac{D}{T}\right) \left(2AT + B - \frac{D}{T^2}\right) \right]$$

$$\frac{\partial f}{\partial p} = \beta = 3,14x10^{-8} Pa^{-1}$$

$$\frac{\partial f}{\partial t} = 2\gamma t$$

$$\frac{\partial X_{v}}{\partial h} = \frac{fP_{sv}}{p}$$
$$\frac{\partial x_{v}}{\partial f} = \frac{hP_{sv}}{p}$$



 $\frac{\partial Z}{\partial p} = \frac{-1}{T} \Big[ a_0 + a_1 t + a_2 t^2 + (b_0 + b_1 t) X_v + (C_0 + C_1 t) X_v^2 \Big] + \frac{2p}{T^2} \Big( d + e x_v^2 \Big)$ 

$$\frac{\partial Z}{\partial T} = \frac{p}{T^2} \Big[ a_0 + a_1 t + a_2 t^2 + (b_0 + b_1 t) X_v + (C_o + C_1 t) X_{V_2} \Big] - \frac{2p^2}{T^3} \Big( d + e x_v^2 \Big)$$

$$\frac{\partial Z}{\partial t} = \frac{-p}{T} \left( a_1 + 2a_2t + b_1 X_v + c 1 X_v^2 \right)$$

$$\frac{\partial Z}{\partial X_{v}} = \frac{-p}{T} \left( b_{0} + b_{1}t + 2c_{o}x_{v} + 2c_{1}tx_{v} \right) + \frac{2p2eX_{v}}{T^{2}}$$

$$\frac{\partial \rho}{\partial p} = \frac{Ma}{ZRT} \left( 1 - Xv \left( 1 - \frac{Mv}{Ma} \right) \right)$$
$$\frac{\partial \rho}{\partial Z} = \frac{-pM_a}{Z^2RT} \left[ 1 - x_v \left[ 1 - \frac{M_v}{M_a} \right] \right]$$
$$\frac{\partial \rho}{\partial T} = \frac{-pM_a}{ZRT^2} \left[ 1 - X_v \left( 1 - \frac{M_v}{M_a} \right) \right]$$
$$\frac{\partial \rho}{\partial X_v} = \frac{-pM_a}{ZRT} \left( 1 - \frac{M_v}{M_a} \right)$$
$$\frac{\partial \rho}{\partial R} = \frac{-pM_a}{ZR^2T} \left[ -Xv \left( 1 - \frac{M_v}{M_a} \right) \right]$$

## **Constant R**

$$C_R = \left(\frac{\partial \rho_a}{\partial R}\right)$$

 $C_R = -0,114203618 kgm^3 j^{-1} mol K$ 

## Equation $C_{ec} = 1$

### **Uncertainty evalation**

$$u_p = \sqrt{\sum_{t} \left[ c_i \cdot u(x_i) \right]^2}$$

#### **Degrees of freedom**

$$v_{ef} = \frac{u_{\gamma}^{4}}{\sum_{t}^{n} \frac{u_{xt}^{4}}{v_{t}}} = \frac{u_{\rho}^{4}}{\frac{u_{p}^{4}}{v_{p}} + \frac{u_{t}^{4}}{v_{t}} + \frac{u_{h}^{4}}{v_{h}} + \frac{u_{R}^{4}}{v_{R}} + \frac{u_{ec}^{4}}{v_{ec}}}$$

**Expanded uncertainty** 

$$U = k \cdot u_p$$

Consider that the atmospheric pressure, temperature and relative humidity are correlated, its uncertainty:

$$u_{p} = \sqrt{\sum_{i} (c_{i} \cdot u(x_{i}))^{2} + 2\sum_{i=1}^{N-1} \sum_{j(i+1)}^{N} c_{i} c_{j} u(x_{i}) u(x_{j}) r(x_{i}, x_{j})}$$

Where :

2

$$r(t,p) = \frac{\frac{1}{n(n-1)} \sum_{k=1}^{n} (t_k - \overline{t}) (p_k - \overline{p})}{s(\overline{t}) s(\overline{p})}$$

$$r(t,h) = \frac{\frac{1}{n(n-1)} \sum_{k=1}^{n} (t_k - \bar{t}) (h_k - \bar{h})}{s(\bar{t}) s(\bar{h})}$$

$$r(p,h) = \frac{\frac{1}{n(n-1)} \sum_{k=1}^{n} (p_k - \overline{p})(h_k - \overline{h})}{s(\overline{p})s(\overline{h})}$$

## Reference

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# Thanks for the attention